

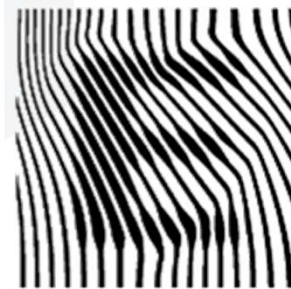


Advanced Electromagnetics:  
21<sup>st</sup> Century Electromagnetics

## Spatially-Variant Planar Gratings

### Lecture Outline

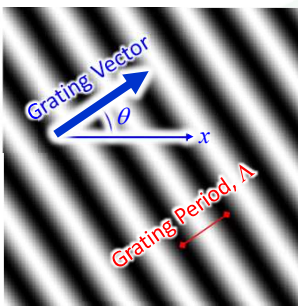
- Preliminary Concepts
  - The grating vector
  - Grating phase
- Generating spatially-variant planar gratings
- Extras
  - More efficient grid strategy
  - Deformation control
  - Spatially-variant planar gratings on curved surfaces



# The Grating Vector $\vec{K}$

Slide 3

## The Grating Vector in Two Dimensions



- The grating vector  $\vec{K}$  is very similar to a wave vector  $\vec{k}$ .
- The direction of  $\vec{K}$  is perpendicular to the grating planes.
- The magnitude of  $\vec{K}$  is  $2\pi$  divided by the period of the grating  $\Lambda$ .

$$|\vec{K}| = \frac{2\pi}{\Lambda}$$

- Given the slant angle  $\theta$ , the grating vector is calculated as

$$\vec{K} = \frac{2\pi}{\Lambda} (\hat{a}_x \cos \theta + \hat{a}_y \sin \theta)$$

- This definition of  $\vec{K}$  allows a convenient calculation of the analog grating.

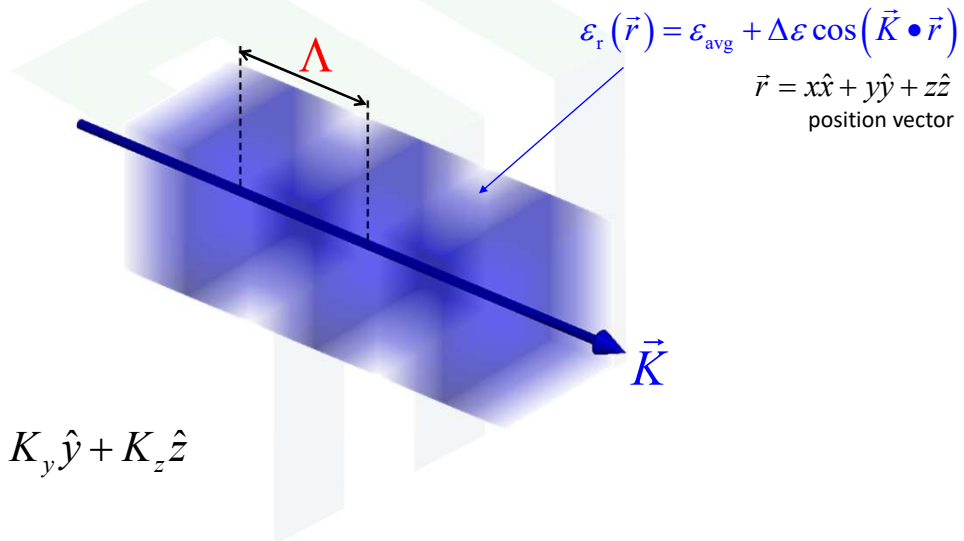
$$\cos(\vec{K} \cdot \vec{r})$$

Slide 4

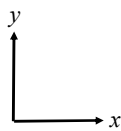
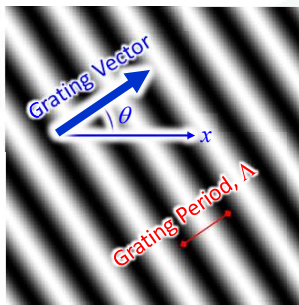
## The Grating Vector in Three Dimensions

$$|\vec{K}| = \frac{2\pi}{\Lambda}$$

$$\vec{K} = K_x \hat{x} + K_y \hat{y} + K_z \hat{z}$$



## The Analog Grating



For simplicity, calculation of the analog grating will be written as

$$\epsilon_a(\vec{r}) = \cos(\vec{K} \cdot \vec{r})$$

or

$$\epsilon_a(\vec{r}) = \text{Re}[\exp(j\vec{K} \cdot \vec{r})]$$

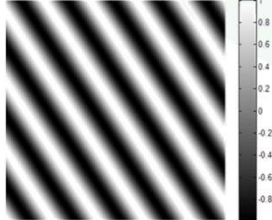
If instead it is desired to generate a physical analog grating, it will need to be scaled to convey permittivity values.

$$\epsilon(\vec{r}) = \epsilon_{\text{avg}} + \Delta\epsilon \cos(\vec{K} \cdot \vec{r})$$

## The Binary Grating

### Analog Grating

$$\epsilon_a(\vec{r}) = \cos(\vec{K} \cdot \vec{r})$$

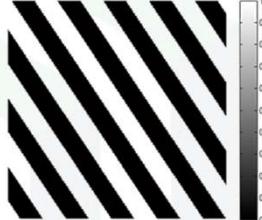


Generation of the grating using a cosine function gives a smooth analog profile.

This requires functionally grading the material properties to realize this. That is hard.

### Binary Grating

$$\epsilon_a(\vec{r}) = \cos(\vec{K} \cdot \vec{r}) > 0$$



Use a threshold to convert the analog profile to a binary grating.

This is much easier to physically realize.

### Controlling the Fill Fraction

$$\epsilon_a(\vec{r}) = \cos(\vec{K} \cdot \vec{r}) > 0.8$$



The threshold value can be adjusted to control the duty cycle, or fill fraction, of the grating.

## Grating Phase

$$\Phi(\vec{r})$$

## Concept of Grating Phase $\Phi(\vec{r})$

An analogy can be made with a standard wave. A wave propagates in the direction of the wave vector  $\vec{k}$ .

$$\vec{E}(\vec{r}) = \vec{E}_0 \cos(\omega t - \vec{k} \cdot \vec{r})$$

As the wave propagates, it accumulates phase  $\phi$  which is a function that increases in the direction of  $\vec{k}$ . The wave could alternatively be calculated just from the phase  $\phi(\vec{r})$ .

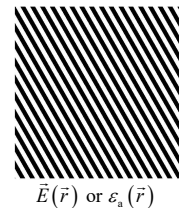
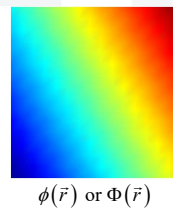
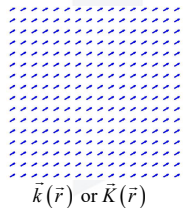
$$\vec{E}(\vec{r}) = \vec{E}_0 \cos[\phi(\vec{r})] \quad \phi(\vec{r}) = \omega t - \vec{k} \cdot \vec{r}$$

For gratings, the grating vector  $\vec{K}$  serves a similar purpose as the wave vector  $\vec{k}$  does for waves.

$$\vec{k}(\vec{r}) \leftrightarrow \vec{K}(\vec{r})$$

$$\phi(\vec{r}) \leftrightarrow \Phi(\vec{r})$$

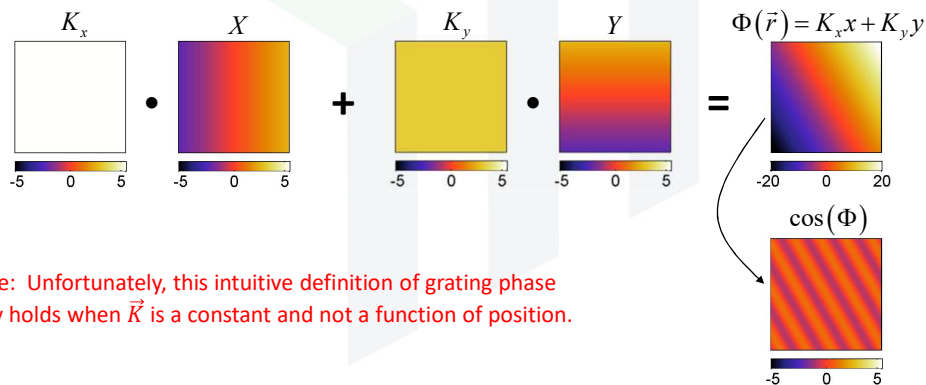
$$\vec{E}(\vec{r}) \leftrightarrow \varepsilon_a(\vec{r})$$



## Definition of Grating Phase

Think of a grating as an unmoving wave because it has almost the same mathematical form. As a wave propagates it accumulates phase. The wave can be calculated from just the phase. Think of the grating phase  $\Phi(\vec{r})$  this way...

$$\varepsilon_a(\vec{r}) = \cos(\vec{K} \cdot \vec{r}) = \cos[\Phi(\vec{r})] \quad \Phi(\vec{r}) = \vec{K} \cdot \vec{r} = K_x x + K_y y$$



## Problem of a Chirped Grating

Suppose the following chirped grating with period  $\Lambda(z)$  is to be generated.

$$\Lambda(z) = \Lambda_0 z \quad 1 \leq z \leq 2$$



This 1D grating is described by the following grating vector function.

$$K(z) = \frac{2\pi}{\Lambda(z)} = \frac{2\pi}{\Lambda_0 z}$$

Now try to calculate the grating using  $\cos(\vec{K} \cdot \vec{r})$ ?

$$\varepsilon_a(z) = \cos[K(z) \cdot z] = \cos\left[\frac{2\pi}{\Lambda_0 z} \cdot z\right] = \cos\left[\frac{2\pi}{\Lambda_0}\right]$$

The argument in the cosine is a constant so no grating is even generated.



## Conclusion From the Chirped Grating

When the grating vector  $\vec{K}(\vec{r})$  is a function of position, the grating can no longer be directly calculated from it.

$$\varepsilon_a(\vec{r}) \neq \cos[\vec{K}(\vec{r}) \cdot \vec{r}] \quad \Phi(\vec{r}) \neq \vec{K}(\vec{r}) \cdot \vec{r}$$

Instead, the grating must be calculated through the intermediate parameter of the grating phase  $\Phi(\vec{r})$ .

$$\varepsilon_a(\vec{r}) = \cos[\Phi(\vec{r})]$$

However, in order to do this a more rigorous definition of grating phase must be adopted.

$$\boxed{\nabla\Phi(\vec{r}) = \vec{K}(\vec{r})} \quad \leftarrow \text{Key equation}$$

## Revised Solution for Chirped Gratings

Now construct the chirped grating using the grating phase.

$$\nabla\Phi = \vec{K}(\vec{r})$$

$$\frac{d\Phi}{dz} = \frac{2\pi}{\Lambda_0 z}$$

$$\Phi(z) = \int_{-\infty}^z \frac{2\pi}{\Lambda_0 z'} dz' = \int_{-\infty}^z \frac{2\pi}{\Lambda_0 z'} dz' + \int_1^z \frac{2\pi}{\Lambda_0 z'} dz' = \frac{2\pi}{\Lambda_0} \ln z' \Big|_1^z$$

$$\Phi(z) = \frac{2\pi}{\Lambda_0} (\ln z - 1)$$

The analog grating is then

$$\varepsilon_a(z) = \cos[\Phi(z)] = \cos\left[\frac{2\pi}{\Lambda_0} (\ln z - 1)\right]$$

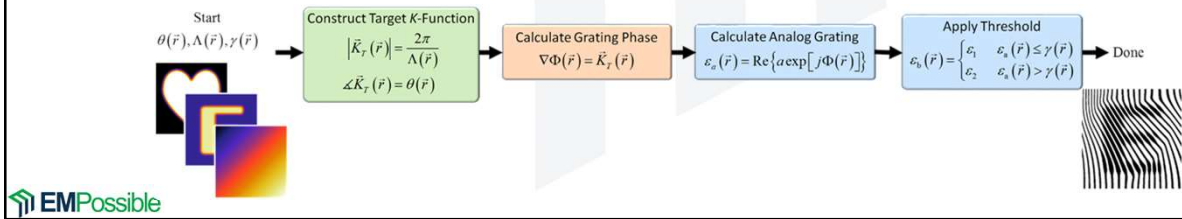


This term is just a constant. Since it is a phase, we are free to choose whatever is convenient. Here we choose zero.

# Generating Spatially-Variant Planar Gratings

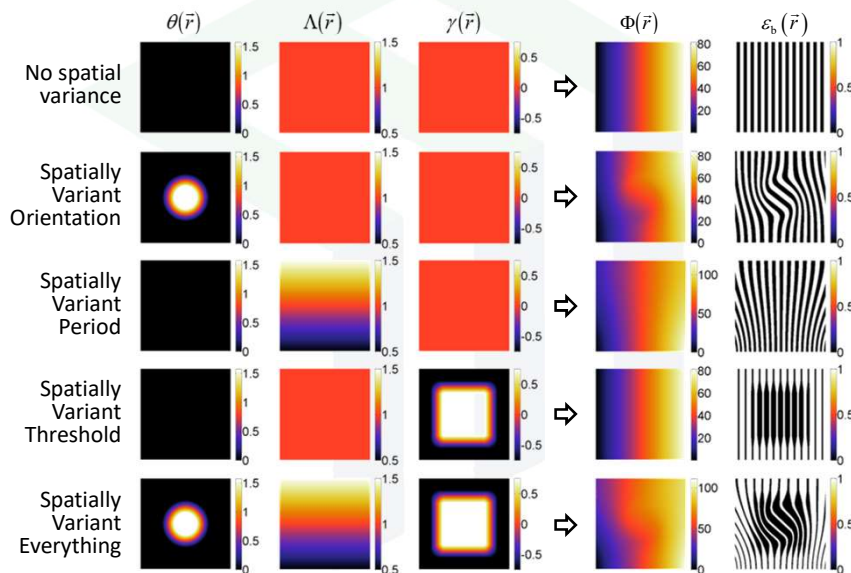
# Procedure for Generating Spatially-Variant Planar Gratings

1. Define the grating vector function  $\vec{K}(\vec{r})$ , or K-function. 
$$\vec{K}(\vec{r}) = \frac{2\pi}{\Lambda(\vec{r})} \left\{ \hat{a}_x \cos[\theta(\vec{r})] + \hat{a}_y \sin[\theta(\vec{r})] \right\}$$
2. Calculate the grating phase  $\Phi(\vec{r})$  from  $\vec{K}(\vec{r})$ . 
$$\nabla\Phi(\vec{r}) = \vec{K}(\vec{r})$$
3. Calculate the analog grating  $\epsilon_a(\vec{r})$  from the grating phase  $\Phi(\vec{r})$ . 
$$\epsilon_a(\vec{r}) = \cos[\Phi(\vec{r})]$$
4. Calculate the binary grating  $\epsilon_b(\vec{r})$  from the analog grating  $\epsilon_a(\vec{r})$ . 
$$\epsilon_b(\vec{r}) = \begin{cases} \epsilon_1 & \epsilon_a(\vec{r}) \leq \gamma(\vec{r}) \\ \epsilon_2 & \epsilon_a(\vec{r}) > \gamma(\vec{r}) \end{cases}$$



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## Spatially-Variant Planar Gratings



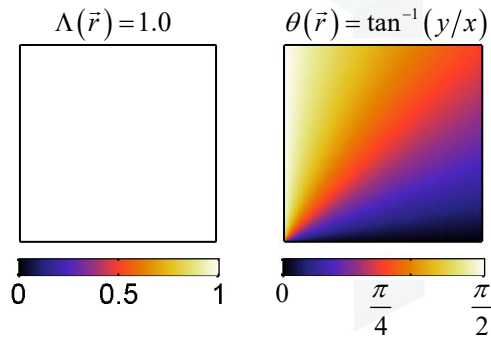
EMPossible

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## Build Input Functions

Two things are needed to build the  $K$ -function:

1. Orientation of the grating as a function of position,  $\theta(\vec{r})$ .
2. Period of the grating as a function of position,  $\Lambda(\vec{r})$ .



```
% GRATING PARAMETERS
a = 1;
er1 = 2.5;
er2 = 1.0;
gth = 0;

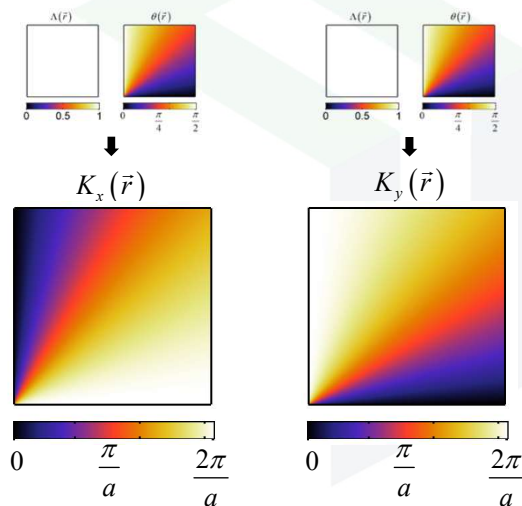
% GRID PARAMETERS
Sx = 5*a;
Sy = Sx;
Nx = 100;
Ny = round(Nx*Sy/Sx);

% CALCULATE GRID
dx = Sx/Nx;
dy = Sy/Ny;
xa = [1:Nx]*dx;
ya = [1:Ny]*dy;
[Y,X] = meshgrid(ya,xa);

% SPATIALLY-VARIANT PARAMETERS
PER = a*ones(Nx,Ny);
THETA = atan2(Y,X);
```

## Calculate the $K$ -Function

The  $K$ -function is calculated directly from the input functions  $\Lambda(\vec{r})$  and  $\theta(\vec{r})$ .



$$K_x(\vec{r}) = \frac{2\pi}{\Lambda(\vec{r})} \cos[\theta(\vec{r})]$$

$$K_y(\vec{r}) = \frac{2\pi}{\Lambda(\vec{r})} \sin[\theta(\vec{r})]$$

```
% CALCULATE K-FUNCTION
Kx = 2*pi./PER.*cos(THETA);
Ky = 2*pi./PER.*sin(THETA);
```

## Finite-Difference Solution to $\nabla\Phi(\vec{r}) = \vec{K}(\vec{r})$

Begin by expanding the governing equation.

$$\nabla\Phi(\vec{r}) = \vec{K}(\vec{r}) \rightarrow \begin{bmatrix} \partial/\partial x \\ \partial/\partial y \\ \partial/\partial z \end{bmatrix} \Phi(\vec{r}) = \begin{bmatrix} K_x(\vec{r}) \\ K_y(\vec{r}) \\ K_z(\vec{r}) \end{bmatrix}$$

Approximate this equation using finite-differences.

$$\begin{bmatrix} \partial/\partial x \\ \partial/\partial y \\ \partial/\partial z \end{bmatrix} \Phi(\vec{r}) = \begin{bmatrix} K_x(\vec{r}) \\ K_y(\vec{r}) \\ K_z(\vec{r}) \end{bmatrix} \rightarrow \begin{bmatrix} \mathbf{D}_x \\ \mathbf{D}_y \\ \mathbf{D}_z \end{bmatrix} \Phi = \begin{bmatrix} \mathbf{k}_x \\ \mathbf{k}_y \\ \mathbf{k}_z \end{bmatrix}$$

Neumann boundary conditions can be used in the derivative operators, but there may exist better boundary conditions to use.

$\Phi$   $\equiv$  column vector containing grating phase throughout grid

$\mathbf{k}_i$   $\equiv$  column vector containing  $K_i$  throughout grid

$\mathbf{D}_i$   $\equiv$  banded matrix that calculates a partial derivative along  $i$ th axis

## More Equations Than Unknowns

The resulting linear algebra problem has more equations than it has unknowns.

$$\begin{bmatrix} \mathbf{D}_x \\ \mathbf{D}_y \\ \mathbf{D}_z \end{bmatrix} \Phi = \begin{bmatrix} \mathbf{k}_x \\ \mathbf{k}_y \\ \mathbf{k}_z \end{bmatrix}$$

$\mathbf{D}_x \Phi = \mathbf{k}_x$   
 $\mathbf{D}_y \Phi = \mathbf{k}_y$   
 $\mathbf{D}_z \Phi = \mathbf{k}_z$

It is usually not possible for the solution to simultaneously satisfy all of the equations.

For this reason, the solution must be a "best fit." One way to do this is to solve it in the sense of least squares.

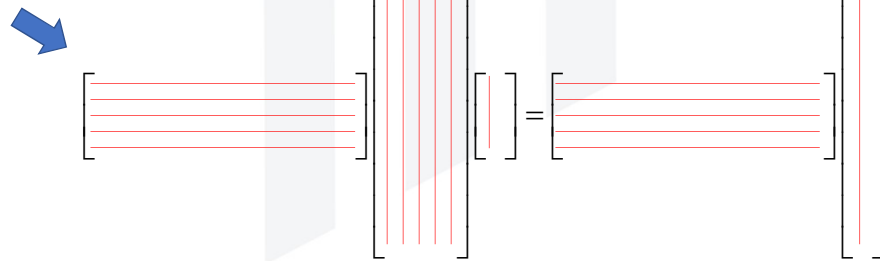
## Solution in the Sense of Least Squares (1 of 2)

First, the problem is cast into the standard form  $\mathbf{Ax} = \mathbf{b}$ .

$$\mathbf{Ax} = \mathbf{b} \quad \mathbf{A} = \begin{bmatrix} \mathbf{D}_x \\ \mathbf{D}_y \\ \mathbf{D}_z \end{bmatrix}, \quad \mathbf{x} = \Phi, \quad \mathbf{b} = \begin{bmatrix} \mathbf{k}_x \\ \mathbf{k}_x \\ \mathbf{k}_x \end{bmatrix}$$

Next, premultiply both sides by  $\mathbf{A}^T$ .

$$\mathbf{A}^T \mathbf{Ax} = \mathbf{A}^T \mathbf{b}$$



## Solution in the Sense of Least Squares (2 of 2)

This is now a new system of equations with the same number of equations as there are unknowns.

$$\mathbf{A}'\mathbf{x} = \mathbf{b}' \quad \longrightarrow \quad \begin{bmatrix} | & | & | \\ \hline | & | & | \\ \hline | & | & | \end{bmatrix} \begin{bmatrix} | \\ | \\ | \end{bmatrix} = \begin{bmatrix} | \\ | \\ | \end{bmatrix}$$

$$\mathbf{A}' = \mathbf{A}^T \mathbf{A}$$

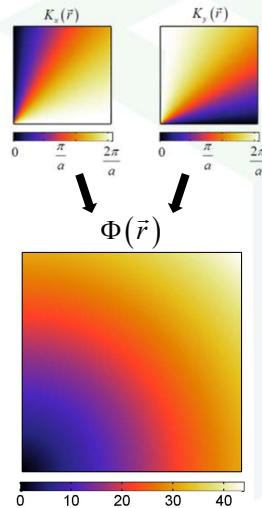
$$\mathbf{b}' = \mathbf{A}^T \mathbf{b}$$

This is solved for  $\mathbf{x}$  using standard linear algebra methods.

$$\mathbf{x} = (\mathbf{A}')^{-1} \mathbf{b}'$$

## Calculate Grating Phase in 2D

We calculate the grating phase  $\Phi(\vec{r})$  from the  $K$ -function as a best fit.



$$\nabla\Phi(\vec{r}) = \vec{K}$$

$$\begin{bmatrix} \mathbf{D}_x \\ \mathbf{D}_y \end{bmatrix} \Phi = \begin{bmatrix} \mathbf{k}_x \\ \mathbf{k}_y \end{bmatrix}$$

```
% CONSTRUCT DERIVATIVE MATRICES
```

```
NS = [Nx Ny];
```

```
RES = [dx dy];
```

```
BC = [1 1];
```

```
[DX,~,DY,~] = fdder(NS,RES,BC);
```

```
% COMPUTE GRATING PHASE
```

```
A = [ DX ; DY ];
```

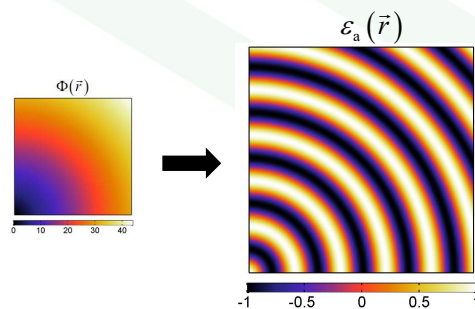
```
b = [ Kx(:) ; Ky(:) ];
```

```
PHI = (A.'*A) \ (A.'*b);
```

```
PHI = reshape(PHI,Nx,Ny);
```

## Calculate Analog Grating

The analog grating  $\epsilon_a(\vec{r})$  is calculated directly from the grating phase  $\Phi(\vec{r})$ .



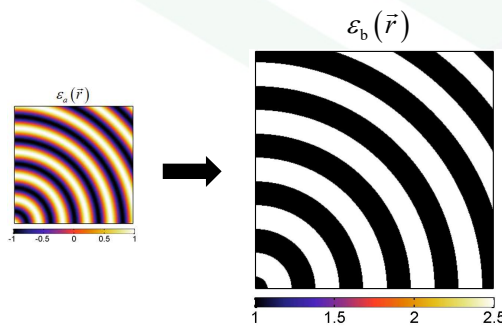
$$\epsilon_a(\vec{r}) = \cos[\Phi(\vec{r})]$$

```
% COMPUTE ANALOG GRATING
```

```
ERA = cos(PHI);
```

## Calculate Binary Grating

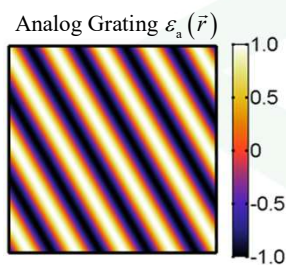
The binary grating  $\varepsilon_b(\vec{r})$  is calculated directly from the analog grating  $\varepsilon_a(\vec{r})$  using the threshold technique and a threshold function  $\gamma(\vec{r})$ .



$$\varepsilon_b(\vec{r}) = \begin{cases} \varepsilon_1 & \varepsilon_a(\vec{r}) \leq \gamma(\vec{r}) \\ \varepsilon_2 & \varepsilon_a(\vec{r}) > \gamma(\vec{r}) \end{cases}$$

```
% COMPUTE BINARY GRATING
ERB = er1*(ERA <= gth) + er2*(ERA > gth);
```

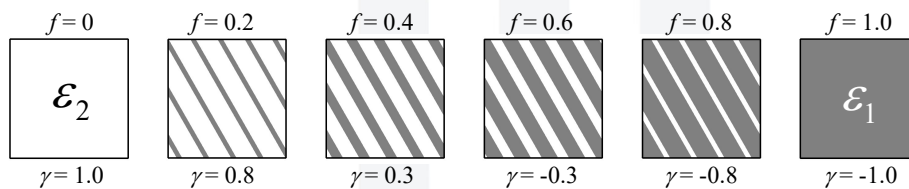
## Controlling Fill Fraction Through the Threshold Function



$$\varepsilon_b(\vec{r}) = \begin{cases} \varepsilon_1 & \varepsilon_a(\vec{r}) \leq \gamma(\vec{r}) \\ \varepsilon_2 & \varepsilon_a(\vec{r}) > \gamma(\vec{r}) \end{cases}$$

Calculate the threshold value in order to realize a given fill factor  $f$  of  $\varepsilon_1$ .

$$\gamma(\vec{r}) = \cos[\pi f(\vec{r})]$$



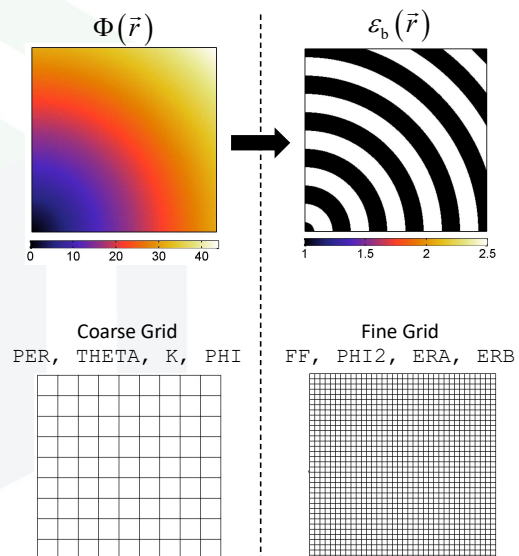
# More Efficient Grid Strategy

Slide 27

## Low-Res / High-Res Grids

Observe how smooth the grating phase function  $\Phi(\vec{r})$  is compared to the final binary grating  $\varepsilon_b(\vec{r})$ .

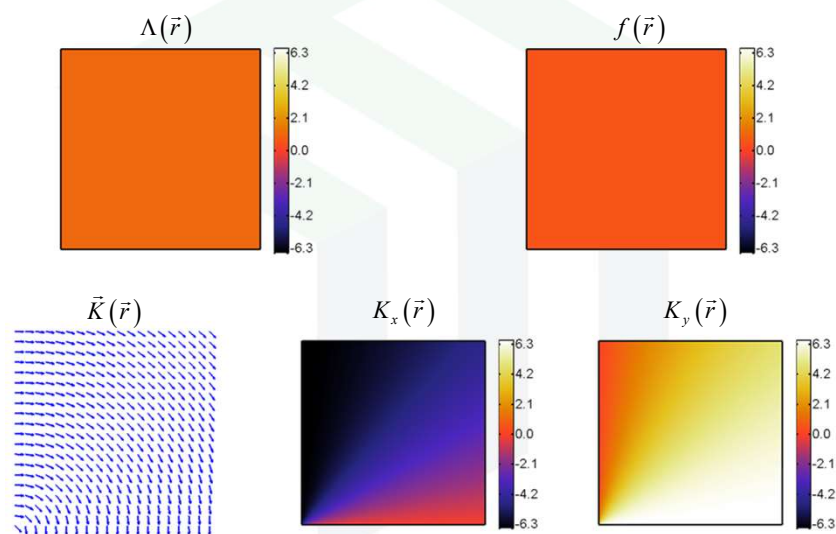
It is usually possible get away with a much coarser grid up to the point where the grating phase is calculated.



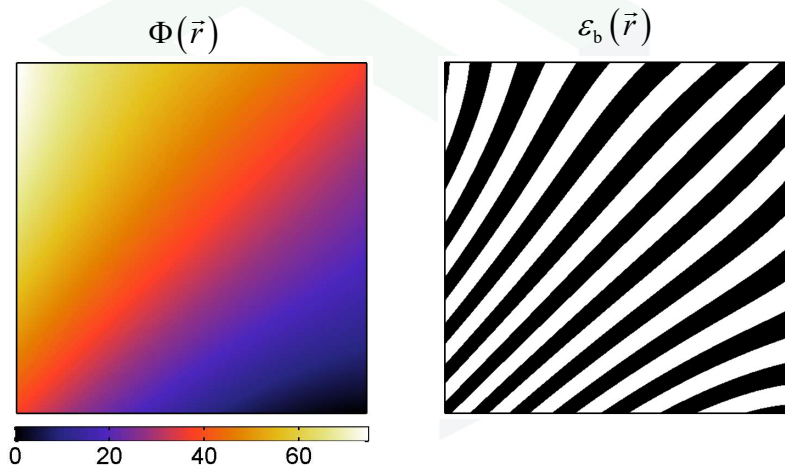
# Deformation Control

Slide 29

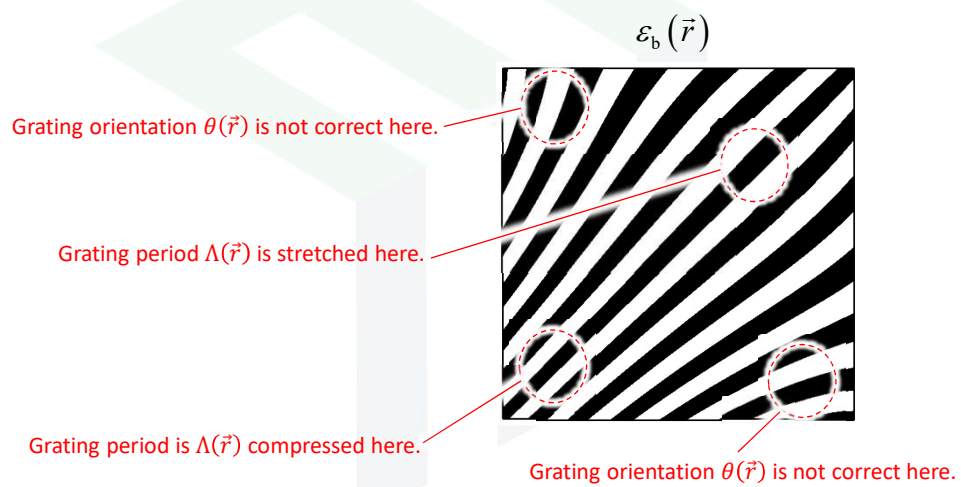
## Typical Input Functions



## Typical Results

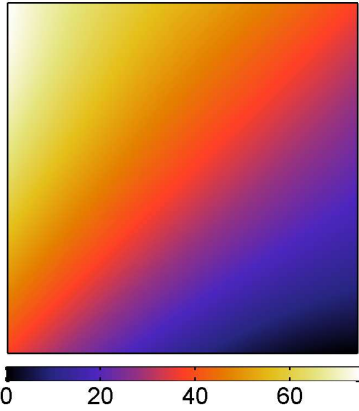


## Typical Problems



# What Grating Was Actually Generated?

$\Phi(\vec{r})$



The process was started with the target  $K$ -function,  $\vec{K}_T(\vec{r})$ .

$$\vec{K}_T(\vec{r}) = \frac{2\pi}{\Lambda(\vec{r})} \left\{ \hat{a}_x \cos[\theta(\vec{r})] + \hat{a}_y \sin[\theta(\vec{r})] \right\}$$

From this, the grating phase  $\Phi(\vec{r})$  was calculated as a best fit.

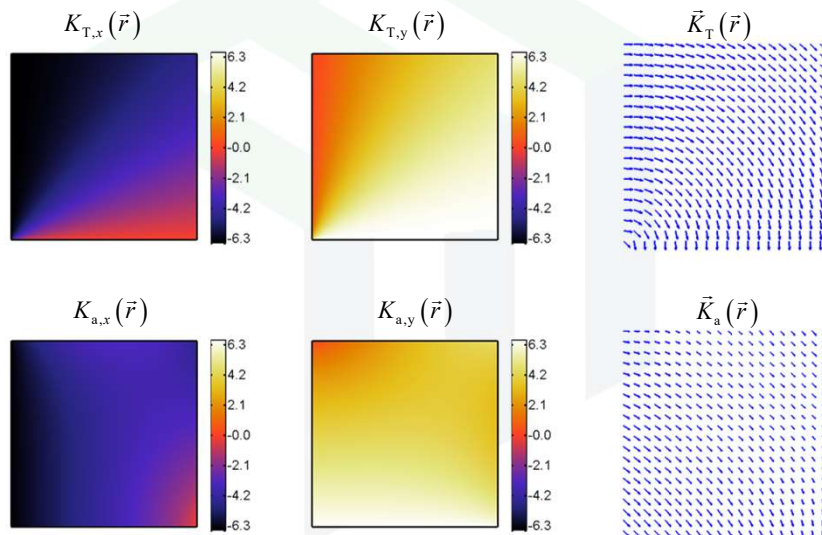
$$\nabla\Phi(\vec{r}) \cong \vec{K}_T(\vec{r})$$

Given the grating phase  $\Phi(\vec{r})$ , the actual  $K$ -function  $\vec{K}_a(\vec{r})$  that was calculated is.

$$\vec{K}_a(\vec{r}) = \nabla\Phi(\vec{r})$$

```
% CALCULATE ACTUAL K-FUNCTION
KA = [DX;DY]*PHI(:);
M = Nx*Ny;
Kxa = KA(1:M);
Kya = KA(M+1:2*M);
Kxa = reshape(Kxa,Nx,Ny);
Kya = reshape(Kya,Nx,Ny);
```

# Comparison of $K$ -Functions



## Quantifying the Problems (1 of 2)

The two parameters quantified by the  $K$ -function  $\vec{K}(\vec{r})$  are the grating period  $\Lambda(\vec{r})$  and the grating orientation  $\theta(\vec{r})$ .

The actual grating period  $\Lambda_a(\vec{r})$  and actual grating orientation  $\theta_a(\vec{r})$  from the actual  $K$ -function  $\vec{K}_a(\vec{r})$ .

$$\Lambda_a(\vec{r}) = \frac{2\pi}{|\vec{K}_a(\vec{r})|}$$

$$\theta_a(\vec{r}) = \tan^{-1} \left[ \frac{K_y(\vec{r})}{K_x(\vec{r})} \right]$$

$$\Delta\Lambda(\vec{r}) = \Lambda(\vec{r}) - \Lambda_a(\vec{r})$$

$$\Delta\theta(\vec{r}) = \theta(\vec{r}) - \theta_a(\vec{r})$$

```
% CALCULATE PROBLEMS
```

```
KMa = sqrt(abs(Kxa).^2 + abs(Kya).^2);
```

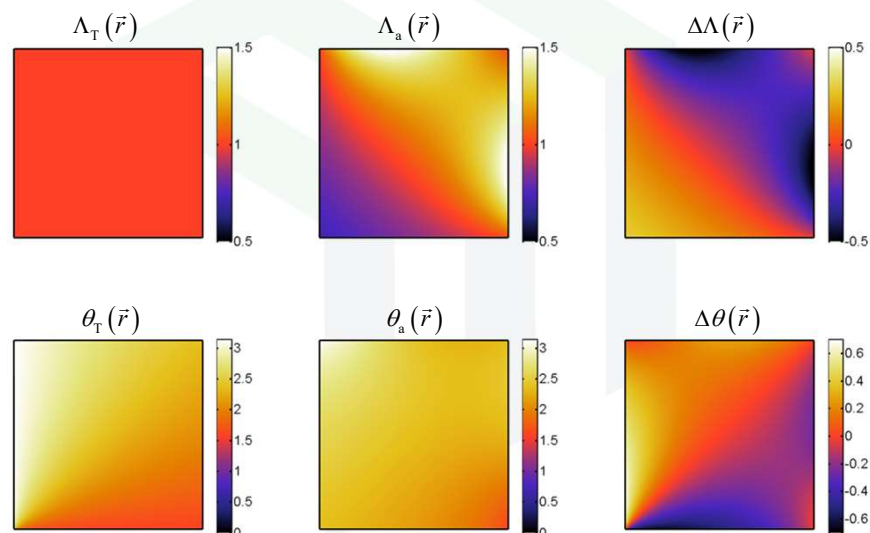
```
PERA = 2*pi./KMa;
```

```
THETAA = atan2(Kya,Kxa);
```

```
DPER = PER - PERA;
```

```
DTHETA = THETA - THETAA;
```

## Quantifying the Problems (2 of 2)



## Four Approaches to Improve the Lattice

1. Improve the grating period  $\Lambda(\vec{r})$  at the cost of the grating orientation  $\theta(\vec{r})$ .
2. Improve the grating orientation  $\theta(\vec{r})$  at the cost of the grating period  $\Lambda(\vec{r})$ .
3. Improve the grating in some parts at the cost of the other parts.
4. Hybrids and weighted combinations of the above approaches.

## Improve Grating Period at the Cost of Grating Orientation (1 of 2)

Step 1 – Compute the target  $K$ -function

$$\vec{K}_T(\vec{r}) = \frac{2\pi}{\Lambda_T(\vec{r})} \left\{ \hat{a}_x \cos[\theta_T(\vec{r})] + \hat{a}_y \sin[\theta_T(\vec{r})] \right\}$$

Step 2 – Solve for the grating phase  $\Phi(\vec{r})$

$$\nabla\Phi(\vec{r}) = \vec{K}_T(\vec{r})$$

Step 3 – Compute the actual functions

$$\vec{K}_a(\vec{r}) = \nabla\Phi(\vec{r}) \quad \Lambda_a(\vec{r}) = \frac{2\pi}{|\vec{K}_a(\vec{r})|} \quad \theta_a(\vec{r}) = \tan^{-1} \left[ \frac{K_y(\vec{r})}{K_x(\vec{r})} \right]$$

Step 4 – Enforce the grating period  $\Lambda(\vec{r})$  in a new  $K$ -function

$$\vec{K}_{\text{new}}(\vec{r}) = \frac{2\pi}{\Lambda_T(\vec{r})} \left\{ \hat{a}_x \cos[\theta_a(\vec{r})] + \hat{a}_y \sin[\theta_a(\vec{r})] \right\}$$

Step 5 – Compute the grating phase  $\Phi(\vec{r})$  from the new  $K$ -function

$$\nabla\Phi(\vec{r}) = \vec{K}_{\text{new}}(\vec{r})$$

Step 6 – If grating has not converged, go back to Step 3.

```

for iter = 1 : NITER
% CALCULATE K-FUNCTION
Kx = 2*pi./PER.*cos(THETA);
Ky = 2*pi./PER.*sin(THETA);

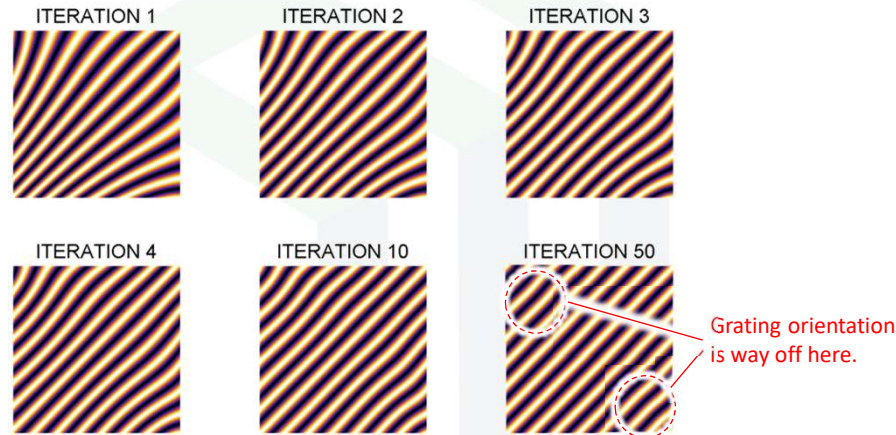
% SOLVE FOR GRATING PHASE
A = [ DX ; DY ];
b = [ Kx(:) ; Ky(:) ];
b = A.*b;
A = A.*A;
PHI = A\b;

% COMPUTE ACTUAL K-FUNCTION
KA = [DX;DY]*PHI(:);
Kxa = KA(1:M);
Kya = KA(M+1:2*M);

% COMPUTE PERIOD AND ANGLE
THETA = atan2(Kya,Kxa);
THETA = reshape(THETA,Nx,Ny);
end

```

## Improve Grating Period at the Cost of Grating Orientation (2 of 2)



Here, convergence is observed after about 10 iterations.  
Notice that orientation has been sacrificed.

## Improve Grating Orientation at the Cost of Grating Period (1 of 2)

Step 1 – Compute the target  $K$ -function

$$\vec{K}_T(\vec{r}) = \frac{2\pi}{\Lambda_T(\vec{r})} \left\{ \hat{a}_x \cos[\theta_T(\vec{r})] + \hat{a}_y \sin[\theta_T(\vec{r})] \right\}$$

Step 2 – Solve for the grating phase  $\Phi(\vec{r})$

$$\nabla\Phi(\vec{r}) = \vec{K}_T(\vec{r})$$

Step 3 – Compute the actual functions

$$\vec{K}_a(\vec{r}) = \nabla\Phi(\vec{r}) \quad \Lambda_a(\vec{r}) = \frac{2\pi}{|\vec{K}_a(\vec{r})|} \quad \theta_a(\vec{r}) = \tan^{-1} \left[ \frac{K_y(\vec{r})}{K_x(\vec{r})} \right]$$

Step 4 – Enforce the grating orientation  $\theta(\vec{r})$  in a new  $K$ -function

$$\vec{K}_{\text{new}}(\vec{r}) = \frac{2\pi}{\Lambda_a(\vec{r})} \left\{ \hat{a}_x \cos[\theta_T(\vec{r})] + \hat{a}_y \sin[\theta_T(\vec{r})] \right\}$$

Step 5 – Compute the grating phase  $\Phi(\vec{r})$  from the new  $K$ -function

$$\nabla\Phi(\vec{r}) = \vec{K}_{\text{new}}(\vec{r})$$

Step 6 – If grating has not converged, go back to Step 3.

```

for iter = 1 : NITER
    % CALCULATE K-FUNCTION
    Kx = 2*pi./PER.*cos(THETA);
    Ky = 2*pi./PER.*sin(THETA);

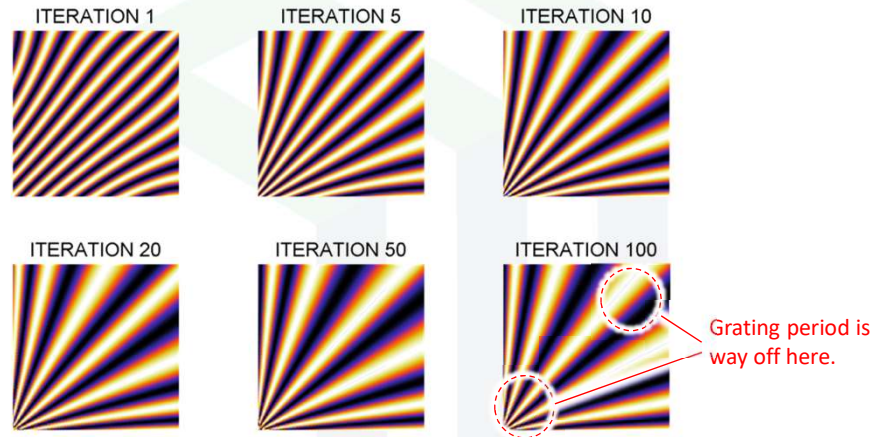
    % COMPUTE GRATING PHASE
    A = [ DX ; DY ];
    b = [ Kx(:) ; Ky(:) ];
    b = A.*b;
    A = A.*A;
    PHI = A\b;

    % COMPUTE ACTUAL K-FUNCTION
    KA = [DX;DY]*PHI(:);
    Kxa = KA(1:M);
    Kya = KA(M+1:2*M);

    % COMPUTE PERIOD AND ANGLE
    KMa = sqrt(abs(Kxa).^2 ...
        + abs(Kya).^2);
    PER = 2*pi./KMa;
    PER = reshape(PER,Nx,Ny);
end

```

## Improve Grating Orientation at the Cost of Grating Period (2 of 2)



Here, convergence is observed after about 50 iterations.  
Notice that period has been sacrificed.

## Improve Grating In Some Regions at the Cost of Other Regions (1 of 2)

Step 1 – Compute the target  $K$ -function

$$\bar{K}_T(\vec{r}) = \frac{2\pi}{\Lambda_T(\vec{r})} \left\{ \hat{a}_x \cos[\theta_T(\vec{r})] + \hat{a}_y \sin[\theta_T(\vec{r})] \right\}$$

Step 2 – Solve for the grating phase  $\Phi(\vec{r})$

$$\nabla\Phi(\vec{r}) = \bar{K}_T(\vec{r})$$

Step 3 – Compute the actual functions

$$\bar{K}_a(\vec{r}) = \nabla\Phi(\vec{r}) \quad \Lambda_a(\vec{r}) = \frac{2\pi}{|\bar{K}_a(\vec{r})|} \quad \theta_a(\vec{r}) = \tan^{-1} \left[ \frac{K_y(\vec{r})}{K_x(\vec{r})} \right]$$

Step 4 – Enforce the grating orientation  $\theta(\vec{r})$  in a new  $K$ -function

$$\bar{K}_{\text{new}}(\vec{r}) = \begin{cases} \bar{K}_T(\vec{r}) & \text{inside of regions to optimize} \\ \bar{K}_a(\vec{r}) & \text{outside of regions to optimize} \end{cases}$$

Step 5 – Compute the grating phase  $\Phi(\vec{r})$  from the new  $K$ -function

$$\nabla\Phi(\vec{r}) = \bar{K}_{\text{new}}(\vec{r})$$

Step 6 – If grating has not converged, go back to Step 3.

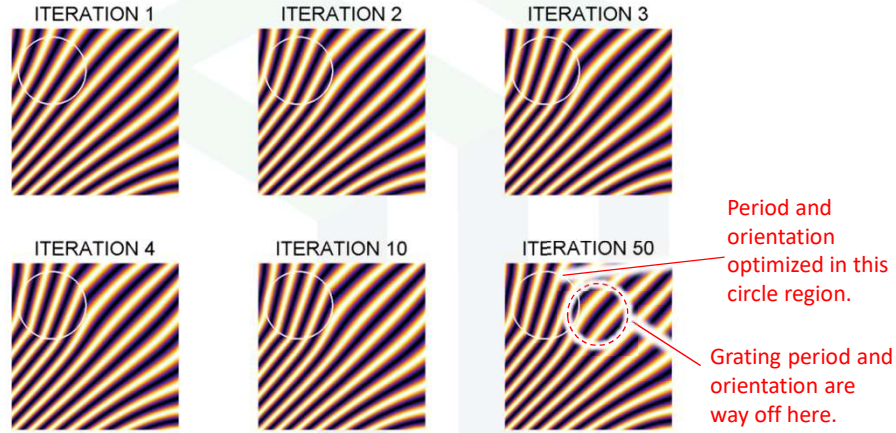
```
% CALCULATE TARGET K-FUNCTION
KTx = 2*pi./PER.*cos(THETA);
KTy = 2*pi./PER.*sin(THETA);
Kx = KTx;
Ky = KTy;

for iter = 1 : NITER
    % COMPUTE GRATING PHASE
    A = [ DX ; DY ];
    b = [ Kx(:) ; Ky(:) ];
    b = A.*b;
    A = A.*A;
    PHI = A\b;

    % COMPUTE ACTUAL K-FUNCTION
    KA = [DX;DY]*PHI(:);
    KAX = KA(1:M);
    KAY = KA(M+1:2*M);

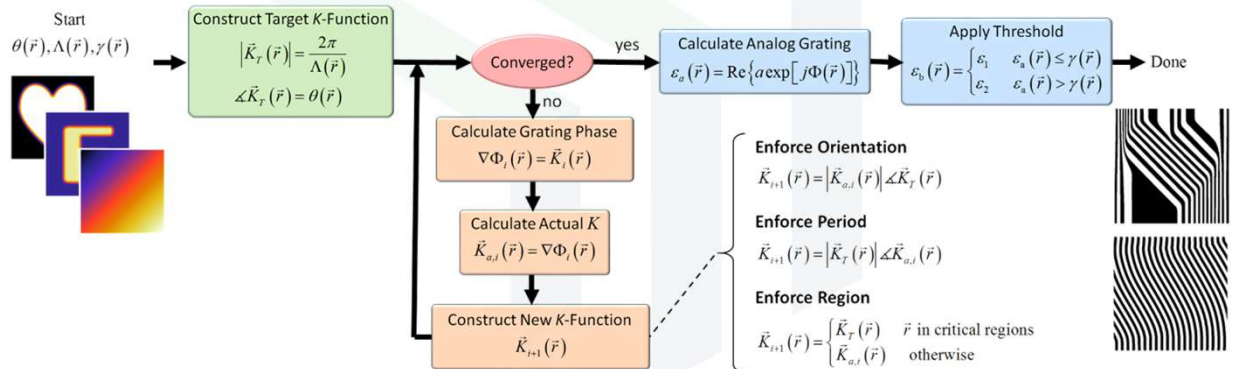
    % ENFORCE CRITICAL REGION R
    KAX = reshape(KAX,Nx,Ny);
    KAY = reshape(KAY,Nx,Ny);
    Kx = KTx.*R + KAX.*(1 - R);
    Ky = KTy.*R + KAY.*(1 - R);
end
```

## Improve Grating In Some Regions at the Cost of Other Regions (2 of 2)



Here, convergence is observed after about 3 iterations. Notice the lattice is most distorted just outside the critical region.

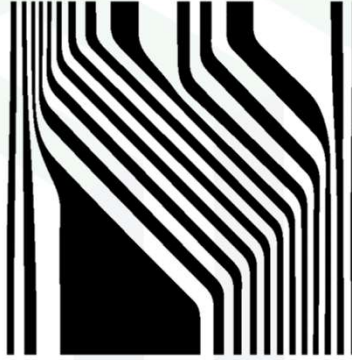
## Block Diagram for Controlling Deformations



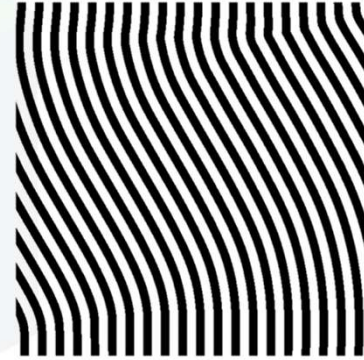
## Another Example



Grating generated from standard algorithm.



Grating generated after enforcing the orientation at the expense of period.



Grating generated after enforcing the period at the expense of orientation.

# Spatially-Variant Planar Gratings on Curved Surfaces

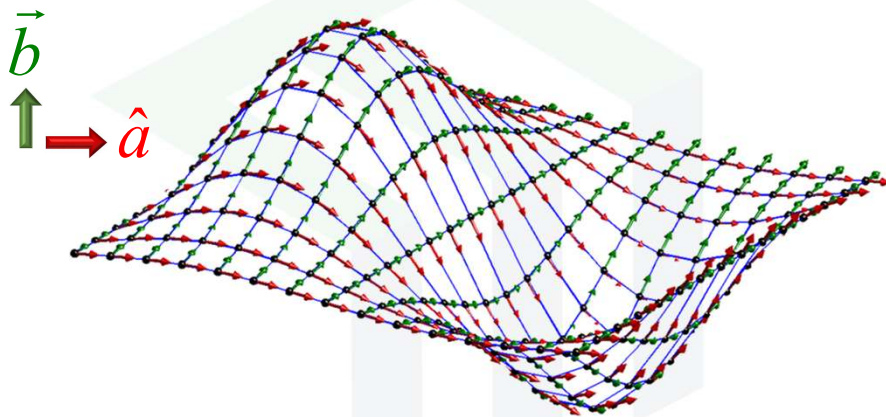
Raymond C. Rumpf, Javier J. Pazos, Jennefir L. Digaum, Stephen M. Kuebler, "Spatially-Variant Periodic Structures in Electromagnetics," accepted for publication in Phil. Trans. A, December 2014.

## The Problem

Suppose it is desired to put a planar grating onto a curved surface without deforming the orientation or period of the grating.

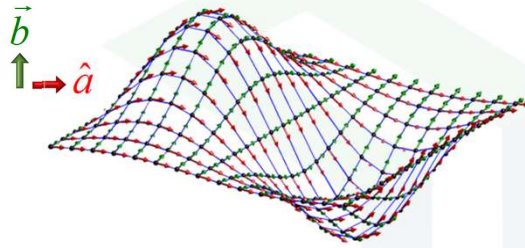
In this case, a grating must be spatially varied in order to not spatially vary it!

## Curved Surface Mesh



On a curved surface, the sense of  $x$  and  $y$  directions must be modified to conform to the curvature. Call these directions  $\hat{a}$  and  $\hat{b}$ . They are defined to always be tangential to the surface.

## Modified Grating Phase Equation

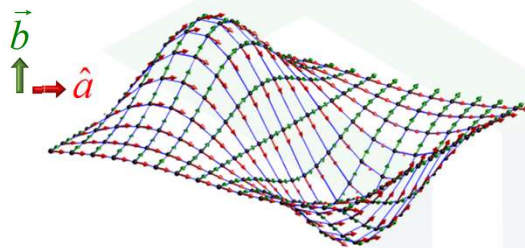


The grating phase equation must be modified to operate on the curved mesh.

$$\nabla' \Phi(\vec{r}) = \vec{K}(\vec{r})$$

$$\nabla' = \frac{\partial}{\partial a} \hat{a} + \frac{\partial}{\partial b} \hat{b}$$

## Modified Finite-Difference Approximation

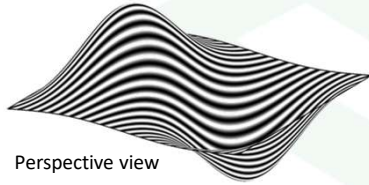


$$\nabla' \Phi(\vec{r}) = \frac{\partial \Phi(\vec{r})}{\partial a} \hat{a} + \frac{\partial \Phi(\vec{r})}{\partial b} \hat{b}$$

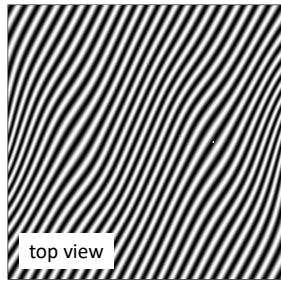
$$\nabla' \Phi(\vec{r}_{p,q}) = \frac{\Phi(\vec{r}_{p+1,q}) - \Phi(\vec{r}_{p-1,q})}{|\vec{r}_{p+1,q} - \vec{r}_{p-1,q}|} \hat{a} + \frac{\Phi(\vec{r}_{p,q+1}) - \Phi(\vec{r}_{p,q-1})}{|\vec{r}_{p,q+1} - \vec{r}_{p,q-1}|} \hat{b}$$

# Example Planar Gratings

Grating #1

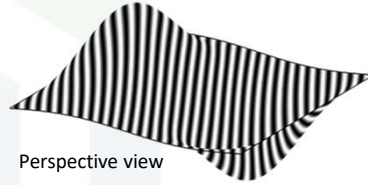


Perspective view

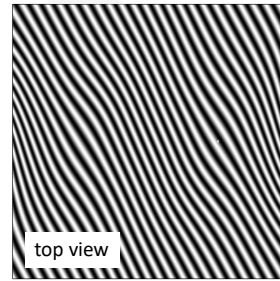


top view

Grating #2



Perspective view



top view