



Computational Science:
Computational Methods in Engineering

Formulation of Slab Waveguide Analysis



Outline

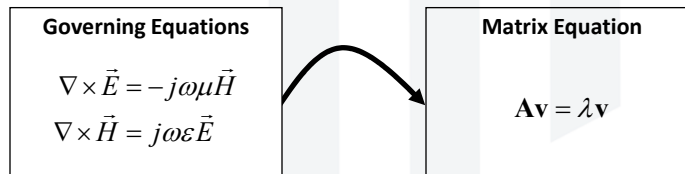
- Formulation
- The Solution



What is Formulation?

Formulation is the initial analytical work done before implementing a computer code.

Usually formulation starts with the governing equation(s) and ends with the matrix equation to be solved.



Formulation

Governing Equations

Since this is an electrodynamics problem, start with Maxwell's curl equations.

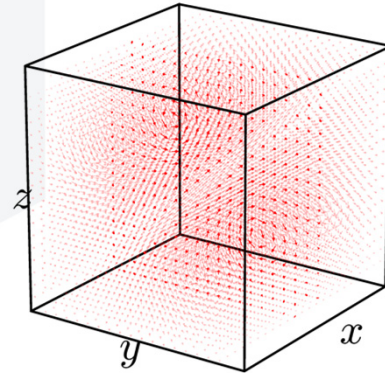
$$\nabla \times \vec{E} = -j\omega\mu\vec{H}$$

$$\nabla \times \vec{H} = j\omega\varepsilon\vec{E}$$

Vector Curl

The curl of a vector is a measure of the vector field's tendency to circulate about an axis. The curl quantity is directly along this axis and the magnitude measures the strength of the circulation.

$$\nabla \times \vec{A} = \left(\frac{\partial A_z}{\partial y} - \frac{\partial A_y}{\partial z} \right) \hat{a}_x + \left(\frac{\partial A_x}{\partial z} - \frac{\partial A_z}{\partial x} \right) \hat{a}_y + \left(\frac{\partial A_y}{\partial x} - \frac{\partial A_x}{\partial y} \right) \hat{a}_z$$



Expand Governing Equations (1 of 2)

Expand the first equation into its vector components.

$$\nabla \times \vec{E} = -j\omega\mu\vec{H}$$

$$\left(\frac{\partial E_z}{\partial y} - \frac{\partial E_y}{\partial z} \right) \hat{a}_x + \left(\frac{\partial E_x}{\partial z} - \frac{\partial E_z}{\partial x} \right) \hat{a}_y + \left(\frac{\partial E_y}{\partial x} - \frac{\partial E_x}{\partial y} \right) \hat{a}_z = -j\omega\mu(H_x \hat{a}_x + H_y \hat{a}_y + H_z \hat{a}_z)$$

$$\left(\frac{\partial E_z}{\partial y} - \frac{\partial E_y}{\partial z} \right) \hat{a}_x + \left(\frac{\partial E_x}{\partial z} - \frac{\partial E_z}{\partial x} \right) \hat{a}_y + \left(\frac{\partial E_y}{\partial x} - \frac{\partial E_x}{\partial y} \right) \hat{a}_z = -j\omega\mu H_x \hat{a}_x - j\omega\mu H_y \hat{a}_y - j\omega\mu H_z \hat{a}_z$$

Expand Governing Equations (1 of 2)

Expand the first equation into its vector components.

$$\nabla \times \vec{E} = -j\omega\mu\vec{H}$$

$$\left(\frac{\partial E_z}{\partial y} - \frac{\partial E_y}{\partial z}\right)\hat{a}_x + \left(\frac{\partial E_x}{\partial z} - \frac{\partial E_z}{\partial x}\right)\hat{a}_y + \left(\frac{\partial E_y}{\partial x} - \frac{\partial E_x}{\partial y}\right)\hat{a}_z = -j\omega\mu(H_x\hat{a}_x + H_y\hat{a}_y + H_z\hat{a}_z)$$

$$\left(\frac{\partial E_z}{\partial y} - \frac{\partial E_y}{\partial z}\right)\hat{a}_x + \left(\frac{\partial E_x}{\partial z} - \frac{\partial E_z}{\partial x}\right)\hat{a}_y + \left(\frac{\partial E_y}{\partial x} - \frac{\partial E_x}{\partial y}\right)\hat{a}_z = -j\omega\mu H_x\hat{a}_x - j\omega\mu H_y\hat{a}_y - j\omega\mu H_z\hat{a}_z$$

The vector components on each side must be equal.

$$\frac{\partial E_z}{\partial y} - \frac{\partial E_y}{\partial z} = -j\omega\mu H_x \quad \frac{\partial E_x}{\partial z} - \frac{\partial E_z}{\partial x} = -j\omega\mu H_y \quad \frac{\partial E_y}{\partial x} - \frac{\partial E_x}{\partial y} = -j\omega\mu H_z$$

Expand Governing Equations (2 of 2)

There are now six coupled partial differential equations.

$$\nabla \times \vec{E} = -j\omega\mu\vec{H}$$

$$\nabla \times \vec{H} = j\omega\epsilon\vec{E}$$

$$\frac{\partial E_z}{\partial y} - \frac{\partial E_y}{\partial z} = -j\omega\mu H_x$$

$$\frac{\partial E_x}{\partial z} - \frac{\partial E_z}{\partial x} = -j\omega\mu H_y$$

$$\frac{\partial E_y}{\partial x} - \frac{\partial E_x}{\partial y} = -j\omega\mu H_z$$

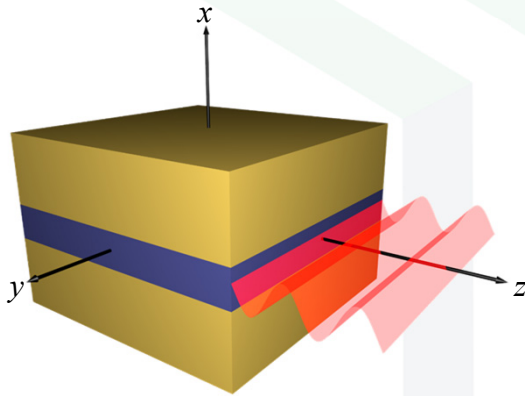
$$\frac{\partial H_z}{\partial y} - \frac{\partial H_y}{\partial z} = j\omega\epsilon E_x$$

$$\frac{\partial H_x}{\partial z} - \frac{\partial H_z}{\partial x} = j\omega\epsilon E_y$$

$$\frac{\partial H_y}{\partial x} - \frac{\partial H_x}{\partial y} = j\omega\epsilon E_z$$

How to Reduce Dimensions

It is always good practice to minimize the number of dimensions utilized in a numerical analysis.



\underline{x}
Material changes as a function of x . The mode profile will change as a function of x . This dimension must be retained.

\underline{y}
Device is uniform. Wave does not propagate in this direction. Mode profile is uniform.

$$\frac{\partial}{\partial y} = 0$$

\underline{z}
Device is uniform. Wave propagates in this direction so wave phase is increasing.

$$\frac{\partial}{\partial z} = -j\beta$$

Apply $\partial/\partial y = 0$

Since nothing is changing in the y direction, any derivative with respect to y must be zero.

$\frac{\partial E_z}{\partial y} - \frac{\partial E_y}{\partial z} = -j\omega\mu H_x$	$-\frac{\partial E_y}{\partial z} = -j\omega\mu H_x$
$\frac{\partial E_x}{\partial z} - \frac{\partial E_z}{\partial x} = -j\omega\mu H_y$	$\frac{\partial E_x}{\partial z} - \frac{\partial E_z}{\partial x} = -j\omega\mu H_y$
$\frac{\partial E_y}{\partial x} - \frac{\partial E_x}{\partial y} = -j\omega\mu H_z$	$\frac{\partial E_y}{\partial x} = -j\omega\mu H_z$
$\frac{\partial H_z}{\partial y} - \frac{\partial H_y}{\partial z} = j\omega\epsilon E_x$	$-\frac{\partial H_y}{\partial z} = j\omega\epsilon E_x$
$\frac{\partial H_x}{\partial z} - \frac{\partial H_z}{\partial x} = j\omega\epsilon E_y$	$\frac{\partial H_x}{\partial z} - \frac{\partial H_z}{\partial x} = j\omega\epsilon E_y$
$\frac{\partial H_y}{\partial x} - \frac{\partial H_x}{\partial y} = j\omega\epsilon E_z$	$\frac{\partial H_y}{\partial x} = j\omega\epsilon E_z$

Two Distinct Mode Types

The revised governing equations have separated into two distinct mode types.

We will analyze the E_y mode

Mode Type 1 – E_y Mode

$$\begin{aligned}\frac{\partial H_x}{\partial z} - \frac{\partial H_z}{\partial x} &= j\omega\epsilon E_y \\ -\frac{\partial E_y}{\partial z} &= -j\omega\mu H_x \\ \frac{\partial E_y}{\partial x} &= -j\omega\mu H_z\end{aligned}$$

Mode Type 2 – H_y Mode

$$\begin{aligned}\frac{\partial E_x}{\partial z} - \frac{\partial E_z}{\partial x} &= -j\omega\mu H_y \\ -\frac{\partial H_y}{\partial z} &= j\omega\epsilon E_x \\ \frac{\partial H_y}{\partial x} &= j\omega\epsilon E_z\end{aligned}$$

$$\begin{aligned}-\frac{\partial E_y}{\partial z} &= -j\omega\mu H_x \\ \frac{\partial E_x}{\partial z} - \frac{\partial E_z}{\partial x} &= -j\omega\mu H_y \\ \frac{\partial E_y}{\partial x} &= -j\omega\mu H_z \\ -\frac{\partial H_y}{\partial z} &= j\omega\epsilon E_x \\ \frac{\partial H_x}{\partial z} - \frac{\partial H_z}{\partial x} &= j\omega\epsilon E_y \\ \frac{\partial H_y}{\partial x} &= j\omega\epsilon E_z\end{aligned}$$

What About $\partial/\partial z$?

The guided mode has the following mathematical form

$$\vec{E}(x, y, z) = \vec{A}(x)e^{-j\beta z}$$

Calculate the partial derivative with respect to z and see what happens.

$$\begin{aligned}\frac{\partial}{\partial z} \vec{E}(x, y, z) &= \frac{\partial}{\partial z} [\vec{A}(x)e^{-j\beta z}] = \vec{A}(x) \frac{\partial}{\partial z} e^{-j\beta z} + e^{-j\beta z} \frac{\partial}{\partial z} \vec{A}(x) \\ &= -j\beta \underbrace{\vec{A}(x)e^{-j\beta z}}_{\vec{E}(x, y, z)} = -j\beta \vec{E}(x, y, z)\end{aligned}$$

It can be concluded that for this slab waveguide analysis,

$$\frac{\partial}{\partial z} = -j\beta$$

1D Governing Equations

The equations for the E_y mode were

$$\begin{aligned}\frac{\partial}{\partial z} H_x - \frac{\partial H_z}{\partial x} &= j\omega\epsilon E_y \\ -\frac{\partial}{\partial z} E_y &= -j\omega\mu H_x \\ \frac{\partial E_y}{\partial x} &= -j\omega\mu H_z\end{aligned}$$

Now replace $\partial/\partial z$ with $-j\beta z$.

$$\begin{aligned}-j\beta H_x - \frac{dH_z}{dx} &= j\omega\epsilon E_y \\ j\beta E_y &= -j\omega\mu H_x \\ \frac{dE_y}{dx} &= -j\omega\mu H_z\end{aligned}$$

The partial derivative has become an ordinary derivative because there is only one independent variable remaining... x .

Normalize the Parameters

Before converting the equations to matrix form, the spatial coordinate x should be normalized to put it in terms of wavelength in some manner.

$$\tilde{x} = \frac{??? x}{\lambda_0}$$

It will be mathematically convenient to normalize by multiplying x by the free space wave number k_0 instead of dividing by just λ_0 .

$$\tilde{x} = k_0 x \quad k_0 = \frac{2\pi}{\lambda_0} = \frac{\omega\sqrt{\mu\epsilon}}{n}$$

Normalizing Maxwell's Equations

Start with the following equation,

$$-j\beta H_x - \frac{dH_z}{dx} = j\omega\epsilon E_y$$

and replace x with \tilde{x}/k_0 .

$$-j\beta H_x - k_0 \frac{dH_z}{d\tilde{x}} = j\omega\epsilon E_y$$

Next, divide both sides of the equation by k_0 .

$$-j \frac{\beta}{k_0} H_x - \frac{dH_z}{d\tilde{x}} = \frac{j\omega\epsilon}{k_0} E_y$$

Recognizing that $\beta = k_0 n_{\text{eff}}$, the equation becomes

$$\begin{aligned} -jn_{\text{eff}} H_x - \frac{dH_z}{d\tilde{x}} &= \frac{j\omega\epsilon}{k_0} E_y \\ &= \frac{j\omega\epsilon_0\epsilon_r}{\omega\sqrt{\mu_0\epsilon_0}} E_y = j\sqrt{\frac{\epsilon_0}{\mu_0}} \epsilon_r E_y \end{aligned}$$

Normalized Equations

Applying the normalizations to all three equations gives

$$\begin{aligned} -jn_{\text{eff}} H_x - \frac{dH_z}{d\tilde{x}} &= j\sqrt{\frac{\epsilon_0}{\mu_0}} \epsilon_r E_y \\ jn_{\text{eff}} E_y &= -j\sqrt{\frac{\mu_0}{\epsilon_0}} \mu_r H_x \\ \frac{dE_y}{d\tilde{x}} &= -j\sqrt{\frac{\mu_0}{\epsilon_0}} \mu_r H_z \end{aligned}$$

Last, at optical frequencies, the magnetic response is negligible so $\mu_r = 1$.

$$\begin{aligned} -jn_{\text{eff}} H_x - \frac{dH_z}{d\tilde{x}} &= j\sqrt{\frac{\epsilon_0}{\mu_0}} \epsilon_r E_y \\ jn_{\text{eff}} E_y &= -j\sqrt{\frac{\mu_0}{\epsilon_0}} H_x \\ \frac{dE_y}{d\tilde{x}} &= -j\sqrt{\frac{\mu_0}{\epsilon_0}} H_z \end{aligned}$$

Final Governing Equation

Solve the last two equations for H_x and H_z .

$$-jn_{\text{eff}}H_x - \frac{dH_z}{d\tilde{x}} = j\sqrt{\frac{\epsilon_0}{\mu_0}}\epsilon_r E_y$$

$$jn_{\text{eff}}E_y = -j\sqrt{\frac{\mu_0}{\epsilon_0}}H_x \rightarrow H_x = -n_{\text{eff}}\sqrt{\frac{\epsilon_0}{\mu_0}}E_y$$

$$\frac{dE_y}{d\tilde{x}} = -j\sqrt{\frac{\mu_0}{\epsilon_0}}H_z \rightarrow H_z = j\sqrt{\frac{\epsilon_0}{\mu_0}}\frac{dE_y}{d\tilde{x}}$$

These are substituted into the first equation to get a single equation containing only E_y . This is why it was called the E_y mode.

$$-jn_{\text{eff}}H_x - \frac{dH_z}{d\tilde{x}} = j\sqrt{\frac{\epsilon_0}{\mu_0}}\epsilon_r E_y$$

$$-jn_{\text{eff}}\left(-n_{\text{eff}}\sqrt{\frac{\epsilon_0}{\mu_0}}E_y\right) - \frac{d}{d\tilde{x}}\left(j\sqrt{\frac{\epsilon_0}{\mu_0}}\frac{dE_y}{d\tilde{x}}\right) = j\sqrt{\frac{\epsilon_0}{\mu_0}}\epsilon_r E_y$$

$$n_{\text{eff}}^2 E_y - \frac{d^2 E_y}{d\tilde{x}^2} = \epsilon_r E_y \rightarrow \frac{d^2 E_y}{d\tilde{x}^2} + \epsilon_r E_y = n_{\text{eff}}^2 E_y$$

Eigen-Value Problem

For optical problems, people like to put everything in terms of refractive index. This is related to the relative permittivity through $\epsilon_r = n^2$.

$$\frac{d^2 E_y}{d\tilde{x}^2} + n^2 E_y = n_{\text{eff}}^2 E_y$$

The governing equation can be rearranged to the form of a standard eigen-value problem $\mathbf{Ax} = \lambda\mathbf{x}$.

$$\left[\frac{d^2}{d\tilde{x}^2} + n^2(x) \right] E_y(x) = n_{\text{eff}}^2 E_y(x)$$

$$\mathbf{A} = \frac{d^2}{d\tilde{x}^2} + n^2(x)$$

$$\mathbf{x} = E_y(x)$$

$$\lambda = n_{\text{eff}}^2$$

Matrix Form

Go term-by-term to write the equation in matrix form.

$$\left[\frac{d^2}{d\tilde{x}^2} + n^2(x) \right] E_y(x) = n_{\text{eff}}^2 E_y(x)$$

$$(\mathbf{D}_{\tilde{x}}^2 + \mathbf{n}^2) \mathbf{e}_y = n_{\text{eff}}^2 \mathbf{e}_y$$

or

$$(\mathbf{D}_{\tilde{x}}^2 + \boldsymbol{\varepsilon}) \mathbf{e}_y = n_{\text{eff}}^2 \mathbf{e}_y$$

Eigen Matrix

Eigen Value

Solution

Solving the Eigen-Value Problem

$$(\mathbf{D}_x^2 + \boldsymbol{\varepsilon}) \mathbf{e}_y = n_{\text{eff}}^2 \mathbf{e}_y \rightarrow \begin{array}{l} \mathbf{V} \equiv \text{Eigen-vector matrix} \\ \boldsymbol{\lambda} \equiv \text{Eigen-value matrix} \end{array}$$

$$\mathbf{V} = \begin{bmatrix} e_y^{(1)}(1) & e_y^{(2)}(1) & \dots & e_y^{(M)}(1) \\ e_y^{(1)}(2) & e_y^{(2)}(2) & & e_y^{(M)}(2) \\ e_y^{(1)}(3) & e_y^{(2)}(3) & & e_y^{(M)}(3) \\ \vdots & \vdots & & \vdots \\ e_y^{(1)}(N_x-1) & e_y^{(2)}(N_x-1) & & e_y^{(M)}(N_x-1) \\ e_y^{(1)}(N_x) & e_y^{(2)}(N_x) & & e_y^{(M)}(N_x) \end{bmatrix}$$

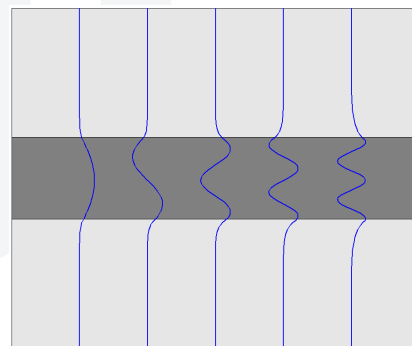
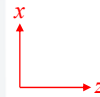
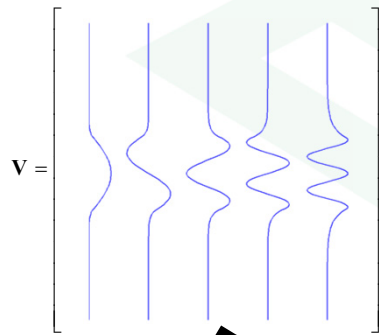
$$\boldsymbol{\lambda} = \begin{bmatrix} (n_{\text{eff}}^{(1)})^2 & & & \\ & (n_{\text{eff}}^{(2)})^2 & & \\ & & \ddots & \\ & & & (n_{\text{eff}}^{(M)})^2 \end{bmatrix}$$

$M = \# \text{ modes}$
Usually $M = N_x$

Eigen-vectors and eigen-values come in pairs.
Do not mix up their pairing!

Visualizing the Solution

The columns of the eigen-vector matrix are pictures of the modes.



The eigen-values are the square of the effective refractive indices of the modes.

$$\lambda = n_{\text{eff}}^2$$