



Computational Science:  
Computational Methods in Engineering

# Formulation of Slab Waveguide Analysis



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## Outline

- Formulation
- The Solution

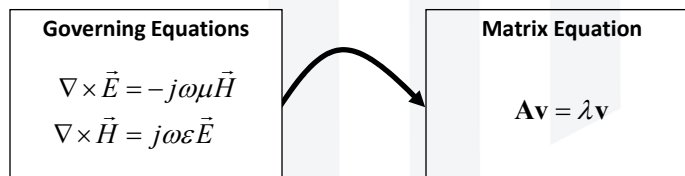


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## What is Formulation?

Formulation is the initial analytical work done before implementing a computer code.

Usually formulation starts with the governing equation(s) and ends with the matrix equation to be solved.



## Formulation

## Governing Equations

Since this is an electrodynamics problem, start with Maxwell's curl equations.

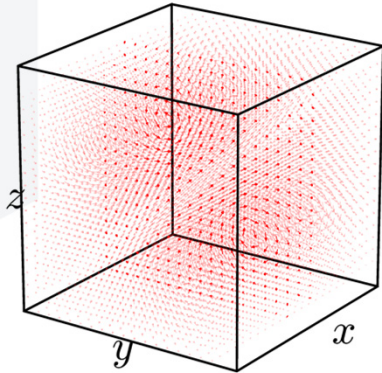
$$\nabla \times \vec{E} = -j\omega\mu\vec{H}$$

$$\nabla \times \vec{H} = j\omega\varepsilon\vec{E}$$

### Vector Curl

The curl of a vector is a measure of the vector field's tendency to circulate about an axis. The curl quantity is directly along this axis and the magnitude measures the strength of the circulation.

$$\nabla \times \vec{A} = \left( \frac{\partial A_z}{\partial y} - \frac{\partial A_y}{\partial z} \right) \hat{a}_x + \left( \frac{\partial A_x}{\partial z} - \frac{\partial A_z}{\partial x} \right) \hat{a}_y + \left( \frac{\partial A_y}{\partial x} - \frac{\partial A_x}{\partial y} \right) \hat{a}_z$$



## Expand Governing Equations (1 of 2)

Expand the first equation into its vector components.

$$\nabla \times \vec{E} = -j\omega\mu\vec{H}$$

$$\left( \frac{\partial E_z}{\partial y} - \frac{\partial E_y}{\partial z} \right) \hat{a}_x + \left( \frac{\partial E_x}{\partial z} - \frac{\partial E_z}{\partial x} \right) \hat{a}_y + \left( \frac{\partial E_y}{\partial x} - \frac{\partial E_x}{\partial y} \right) \hat{a}_z = -j\omega\mu(H_x \hat{a}_x + H_y \hat{a}_y + H_z \hat{a}_z)$$

$$\left( \frac{\partial E_z}{\partial y} - \frac{\partial E_y}{\partial z} \right) \hat{a}_x + \left( \frac{\partial E_x}{\partial z} - \frac{\partial E_z}{\partial x} \right) \hat{a}_y + \left( \frac{\partial E_y}{\partial x} - \frac{\partial E_x}{\partial y} \right) \hat{a}_z = -j\omega\mu H_x \hat{a}_x - j\omega\mu H_y \hat{a}_y - j\omega\mu H_z \hat{a}_z$$

## Expand Governing Equations (1 of 2)

Expand the first equation into its vector components.

$$\nabla \times \vec{E} = -j\omega\mu\vec{H}$$

$$\left(\frac{\partial E_z}{\partial y} - \frac{\partial E_y}{\partial z}\right)\hat{a}_x + \left(\frac{\partial E_x}{\partial z} - \frac{\partial E_z}{\partial x}\right)\hat{a}_y + \left(\frac{\partial E_y}{\partial x} - \frac{\partial E_x}{\partial y}\right)\hat{a}_z = -j\omega\mu(H_x\hat{a}_x + H_y\hat{a}_y + H_z\hat{a}_z)$$

$$\left(\frac{\partial E_z}{\partial y} - \frac{\partial E_y}{\partial z}\right)\hat{a}_x + \left(\frac{\partial E_x}{\partial z} - \frac{\partial E_z}{\partial x}\right)\hat{a}_y + \left(\frac{\partial E_y}{\partial x} - \frac{\partial E_x}{\partial y}\right)\hat{a}_z = -j\omega\mu H_x\hat{a}_x - j\omega\mu H_y\hat{a}_y - j\omega\mu H_z\hat{a}_z$$

The vector components on each side must be equal.

$$\frac{\partial E_z}{\partial y} - \frac{\partial E_y}{\partial z} = -j\omega\mu H_x \quad \frac{\partial E_x}{\partial z} - \frac{\partial E_z}{\partial x} = -j\omega\mu H_y \quad \frac{\partial E_y}{\partial x} - \frac{\partial E_x}{\partial y} = -j\omega\mu H_z$$

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## Expand Governing Equations (2 of 2)

There are now six coupled partial differential equations.

$$\nabla \times \vec{E} = -j\omega\mu\vec{H}$$

$$\nabla \times \vec{H} = j\omega\epsilon\vec{E}$$

$$\frac{\partial E_z}{\partial y} - \frac{\partial E_y}{\partial z} = -j\omega\mu H_x$$

$$\frac{\partial E_x}{\partial z} - \frac{\partial E_z}{\partial x} = -j\omega\mu H_y$$

$$\frac{\partial E_y}{\partial x} - \frac{\partial E_x}{\partial y} = -j\omega\mu H_z$$

$$\frac{\partial H_z}{\partial y} - \frac{\partial H_y}{\partial z} = j\omega\epsilon E_x$$

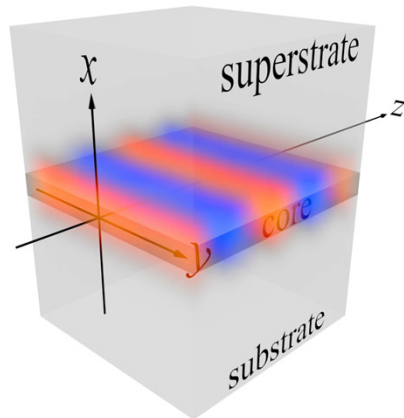
$$\frac{\partial H_x}{\partial z} - \frac{\partial H_z}{\partial x} = j\omega\epsilon E_y$$

$$\frac{\partial H_y}{\partial x} - \frac{\partial H_x}{\partial y} = j\omega\epsilon E_z$$

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## How to Reduce Dimensions

It is always good practice to minimize the number of dimensions utilized in a numerical analysis.



$\underline{x}$   
Material changes as a function of  $x$ . The mode profile will change as a function of  $x$ . This dimension must be retained.

$\underline{y}$   
Device is uniform. Wave does not propagate in this direction. Mode profile is uniform.

$$\frac{\partial}{\partial y} = 0$$

$\underline{z}$   
Device is uniform. Wave propagates in this direction so wave phase is increasing.

$$\frac{\partial}{\partial z} = -j\beta$$

## Apply $\partial/\partial y = 0$

Since nothing is changing in the  $y$  direction, any derivative with respect to  $y$  must be zero.

$$\begin{array}{l}
 \cancel{\frac{\partial E_z}{\partial y}} - \frac{\partial E_y}{\partial z} = -j\omega\mu H_x \\
 \frac{\partial E_x}{\partial z} - \frac{\partial E_z}{\partial x} = -j\omega\mu H_y \\
 \frac{\partial E_y}{\partial x} - \cancel{\frac{\partial E_x}{\partial y}} = -j\omega\mu H_z \\
 \\
 \cancel{\frac{\partial H_z}{\partial y}} - \frac{\partial H_y}{\partial z} = j\omega\varepsilon E_x \\
 \frac{\partial H_x}{\partial z} - \frac{\partial H_z}{\partial x} = j\omega\varepsilon E_y \\
 \frac{\partial H_y}{\partial x} - \cancel{\frac{\partial H_x}{\partial y}} = j\omega\varepsilon E_z
 \end{array}
 \quad \longrightarrow \quad
 \begin{array}{l}
 -\frac{\partial E_y}{\partial z} = -j\omega\mu H_x \\
 \frac{\partial E_x}{\partial z} - \frac{\partial E_z}{\partial x} = -j\omega\mu H_y \\
 \frac{\partial E_y}{\partial x} = -j\omega\mu H_z \\
 \\
 -\frac{\partial H_y}{\partial z} = j\omega\varepsilon E_x \\
 \frac{\partial H_x}{\partial z} - \frac{\partial H_z}{\partial x} = j\omega\varepsilon E_y \\
 \frac{\partial H_y}{\partial x} = j\omega\varepsilon E_z
 \end{array}$$

## Two Distinct Mode Types

The revised governing equations have separated into two distinct mode types.

*E* mode will be analyzed here

$$-\frac{\partial E_y}{\partial z} = -j\omega\mu H_x$$

$$\frac{\partial E_x}{\partial z} - \frac{\partial E_z}{\partial x} = -j\omega\mu H_y$$

$$\frac{\partial E_y}{\partial x} = -j\omega\mu H_z$$

$$-\frac{\partial H_y}{\partial z} = j\omega\varepsilon E_x$$

$$\frac{\partial H_x}{\partial z} - \frac{\partial H_z}{\partial x} = j\omega\varepsilon E_y$$

$$\frac{\partial H_y}{\partial x} = j\omega\varepsilon E_z$$

Mode Type 1 – E Mode

$$\frac{\partial H_x}{\partial z} - \frac{\partial H_z}{\partial x} = j\omega\varepsilon E_y$$

$$-\frac{\partial E_y}{\partial z} = -j\omega\mu H_x$$

$$\frac{\partial E_y}{\partial x} = -j\omega\mu H_z$$

Mode Type 2 – H Mode

$$\frac{\partial E_x}{\partial z} - \frac{\partial E_z}{\partial x} = -j\omega\mu H_y$$

$$-\frac{\partial H_y}{\partial z} = j\omega\varepsilon E_x$$

$$\frac{\partial H_y}{\partial x} = j\omega\varepsilon E_z$$

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## What About $\partial/\partial z$ ?

The guided mode has the following mathematical form

$$\vec{E}(x, y, z) = \vec{A}(x)e^{-j\beta z}$$

Calculate the partial derivative with respect to  $z$  and see what happens.

$$\begin{aligned} \frac{\partial}{\partial z} \vec{E}(x, y, z) &= \frac{\partial}{\partial z} [\vec{A}(x)e^{-j\beta z}] = \vec{A}(x) \frac{\partial}{\partial z} e^{-j\beta z} + e^{-j\beta z} \frac{\partial}{\partial z} \vec{A}(x) = -j\beta \underbrace{\vec{A}(x)e^{-j\beta z}}_{\vec{E}(x, y, z)} \\ &= -j\beta \vec{E}(x, y, z) \end{aligned}$$

It can be concluded that for this slab waveguide analysis,

$$\frac{\partial}{\partial z} = -j\beta$$

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## 1D Governing Equations

The equations for the  $E$  mode were

$$\begin{aligned}\frac{\partial}{\partial z} H_x - \frac{\partial H_z}{\partial x} &= j\omega\epsilon E_y \\ -\frac{\partial}{\partial z} E_y &= -j\omega\mu H_x \\ \frac{\partial E_y}{\partial x} &= -j\omega\mu H_z\end{aligned}$$

Now replace  $\partial/\partial z$  with  $-j\beta z$ .

$$\begin{aligned}-j\beta H_x - \frac{dH_z}{dx} &= j\omega\epsilon E_y \\ j\beta E_y &= -j\omega\mu H_x \\ \frac{dE_y}{dx} &= -j\omega\mu H_z\end{aligned}$$

The partial derivative has become an ordinary derivative because there is only one independent variable remaining... $x$ .

## Normalize the Grid Coordinate(s)

Before converting the equations to matrix form, the spatial coordinate  $x$  should be normalized to put it in terms of the free space wavelength  $\lambda_0$  in some manner.

$$\tilde{x} = \frac{??? x}{\lambda_0}$$

It will be mathematically convenient to normalize  $x$  by multiplying by the free space wave number  $k_0$  instead of dividing by  $\lambda_0$ .

$$\tilde{x} = k_0 x$$

$$k_0 = \frac{2\pi}{\lambda_0}$$

However, multiplying by  $k_0$  also scales  $x$  by a factor of  $2\pi$ .

Observe that multiplying by  $k_0$  is still dividing by  $\lambda_0$ .

## Normalizing Maxwell's Equations

Start with the following equation,

$$-j\beta H_x - \frac{dH_z}{dx} = j\omega\epsilon E_y$$

and replace  $x$  with  $\tilde{x}/k_0$ .

$$-j\beta H_x - k_0 \frac{dH_z}{d\tilde{x}} = j\omega\epsilon E_y$$

Next, divide both sides of the equation by  $k_0$ .

$$-j \frac{\beta}{k_0} H_x - \frac{dH_z}{d\tilde{x}} = \frac{j\omega\epsilon}{k_0} E_y$$

Recognizing that  $\beta = k_0 n_{\text{eff}}$ , the equation becomes

$$-jn_{\text{eff}} H_x - \frac{dH_z}{d\tilde{x}} = \frac{j\omega\epsilon}{k_0} E_y = \frac{j\omega\epsilon_0\epsilon_r}{\omega\sqrt{\mu_0\epsilon_0}} E_y = j\sqrt{\frac{\epsilon_0}{\mu_0}} \epsilon_r E_y$$

## Normalize All E Mode Equations

Applying the normalizations to all three equations gives

$$-jn_{\text{eff}} H_x - \frac{dH_z}{d\tilde{x}} = j\sqrt{\frac{\epsilon_0}{\mu_0}} \epsilon_r E_y$$

$$jn_{\text{eff}} E_y = -j\sqrt{\frac{\mu_0}{\epsilon_0}} \mu_r H_x$$

$$\frac{dE_y}{d\tilde{x}} = -j\sqrt{\frac{\mu_0}{\epsilon_0}} \mu_r H_z$$

Last, at optical frequencies, the magnetic response is negligible so  $\mu_r = 1$ .

$$-jn_{\text{eff}} H_x - \frac{dH_z}{d\tilde{x}} = j\sqrt{\frac{\epsilon_0}{\mu_0}} \epsilon_r E_y$$

$$jn_{\text{eff}} E_y = -j\sqrt{\frac{\mu_0}{\epsilon_0}} H_x$$

$$\frac{dE_y}{d\tilde{x}} = -j\sqrt{\frac{\mu_0}{\epsilon_0}} H_z$$

## Final Governing Equation

Solve the last two equations for  $H_x$  and  $H_z$ .

$$-jn_{\text{eff}}H_x - \frac{dH_z}{d\tilde{x}} = j\sqrt{\frac{\epsilon_0}{\mu_0}}\epsilon_r E_y$$

$$jn_{\text{eff}}E_y = -j\sqrt{\frac{\mu_0}{\epsilon_0}}H_x \rightarrow H_x = -n_{\text{eff}}\sqrt{\frac{\epsilon_0}{\mu_0}}E_y$$

$$\frac{dE_y}{d\tilde{x}} = -j\sqrt{\frac{\mu_0}{\epsilon_0}}H_z \rightarrow H_z = j\sqrt{\frac{\epsilon_0}{\mu_0}}\frac{dE_y}{d\tilde{x}}$$

These are substituted into the first equation to get a single equation containing only  $E_y$ . This is why it was called the  $E$  mode.

$$-jn_{\text{eff}}\left(-n_{\text{eff}}\sqrt{\frac{\epsilon_0}{\mu_0}}E_y\right) - \frac{d}{d\tilde{x}}\left(j\sqrt{\frac{\epsilon_0}{\mu_0}}\frac{dE_y}{d\tilde{x}}\right) = j\sqrt{\frac{\epsilon_0}{\mu_0}}\epsilon_r E_y$$

$$n_{\text{eff}}^2 E_y - \frac{d^2 E_y}{d\tilde{x}^2} = \epsilon_r E_y \longrightarrow \frac{d^2 E_y}{d\tilde{x}^2} + \epsilon_r E_y = n_{\text{eff}}^2 E_y$$

## Eigen-Value Problem

For optical problems, people like to put everything in terms of refractive index  $n$  instead of relative permittivity  $\epsilon_r$ . These are related through  $\epsilon_r = n^2$ .

$$\frac{d^2 E_y}{d\tilde{x}^2} + n^2 E_y = n_{\text{eff}}^2 E_y$$

The governing equation is rearranged to the form of a standard eigen-value problem  $\mathbf{Ax} = \lambda\mathbf{x}$ .

$$\left[ \frac{d^2}{d\tilde{x}^2} + n^2(x) \right] E_y(x) = n_{\text{eff}}^2 E_y(x)$$

$$\mathbf{A} = \frac{d^2}{d\tilde{x}^2} + n^2(x)$$

$$\mathbf{x} = E_y(x)$$

$$\lambda = n_{\text{eff}}^2$$

## Matrix Form

Go term-by-term to write the equation in matrix form.

$$\left[ \frac{d^2}{d\tilde{x}^2} + n^2(x) \right] E_y(x) = n_{\text{eff}}^2 E_y(x)$$

$$(\mathbf{D}_{\tilde{x}}^2 + \mathbf{n}^2) \mathbf{e}_y = n_{\text{eff}}^2 \mathbf{e}_y$$

or

$$(\mathbf{D}_{\tilde{x}}^2 + \boldsymbol{\varepsilon}) \mathbf{e}_y = n_{\text{eff}}^2 \mathbf{e}_y$$

Eigen Matrix

Eigen Value

## Solution

## Solving the Eigen-Value Problem

$$(\mathbf{D}_x^2 + \boldsymbol{\varepsilon}) \mathbf{e}_y = n_{\text{eff}}^2 \mathbf{e}_y \rightarrow \begin{array}{l} \mathbf{V} \equiv \text{Eigen-vector matrix} \\ \boldsymbol{\lambda} \equiv \text{Eigen-value matrix} \end{array}$$

$$\mathbf{V} = \begin{bmatrix} e_y^{(1)}(1) & e_y^{(2)}(1) & \dots & e_y^{(M)}(1) \\ e_y^{(1)}(2) & e_y^{(2)}(2) & & e_y^{(M)}(2) \\ e_y^{(1)}(3) & e_y^{(2)}(3) & & e_y^{(M)}(3) \\ \vdots & \vdots & & \vdots \\ e_y^{(1)}(N_x-1) & e_y^{(2)}(N_x-1) & & e_y^{(M)}(N_x-1) \\ e_y^{(1)}(N_x) & e_y^{(2)}(N_x) & & e_y^{(M)}(N_x) \end{bmatrix}$$

$M = \# \text{ modes}$   
Usually  $M = N_x$

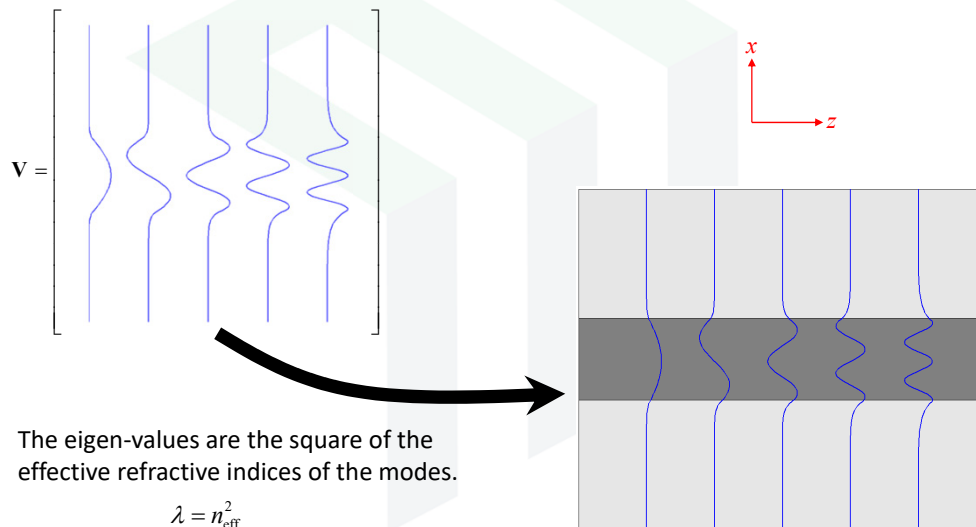
$$\boldsymbol{\lambda} = \begin{bmatrix} (n_{\text{eff}}^{(1)})^2 & & & \\ & (n_{\text{eff}}^{(2)})^2 & & \\ & & \ddots & \\ & & & (n_{\text{eff}}^{(M)})^2 \end{bmatrix}$$

Eigen-vectors and eigen-values come in pairs.  
Do not mix up their pairing!

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## Visualizing the Solution

The columns of the eigen-vector matrix are pictures of the modes.



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